

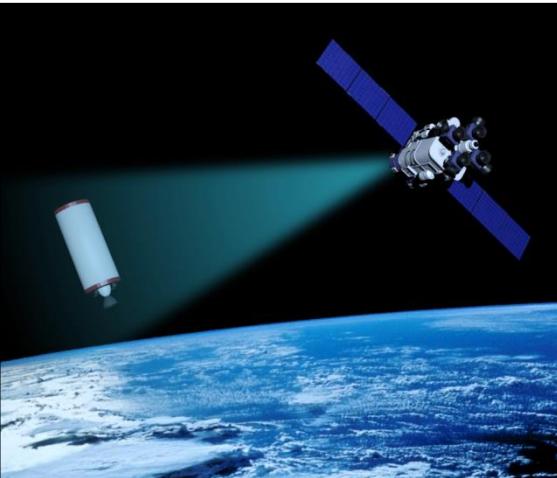


Attitude dynamics and control of space object during contactless transportation by ion beam

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Outline



- Introduction
- Mathematical model
- Equilibrium state
- Uncontrolled attitude motion
- Ion beam thrust control
- Results of numerical simulation
- Conclusions and results

Introduction



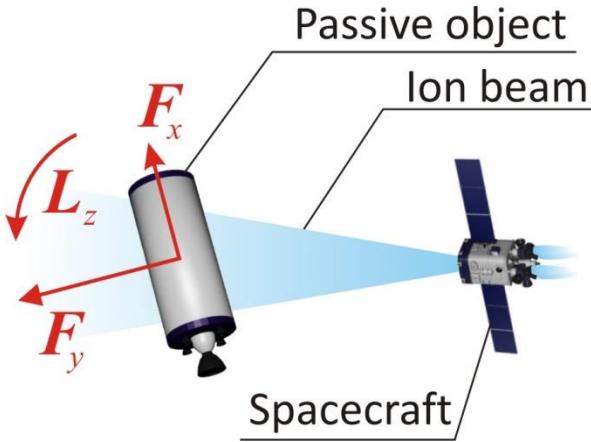
Application of contactless systems

- space debris removal
- serving long-lived satellites
- putting satellites into working orbits
- deflection of asteroids

Ion beam transportation systems

- ease of implementation,
- versatility
- safety

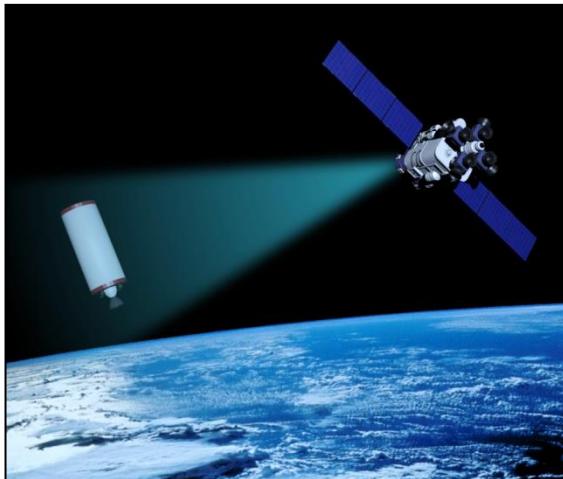
Introduction



The aims of this work

- study of a spatial motion dynamics of a passive space object under the influence of ion beam;
- development of the control law providing stabilization of the object oscillations.

Mathematical model. Assumptions



- Spacecraft is a mass point
- Passive object is a axisymmetric homogeneous cylinder
- Spacecraft's control system provides a constant distance between the object and the spacecraft
- Only ion and gravitational forces and torques act on the system

Mathematical model. Reference frames

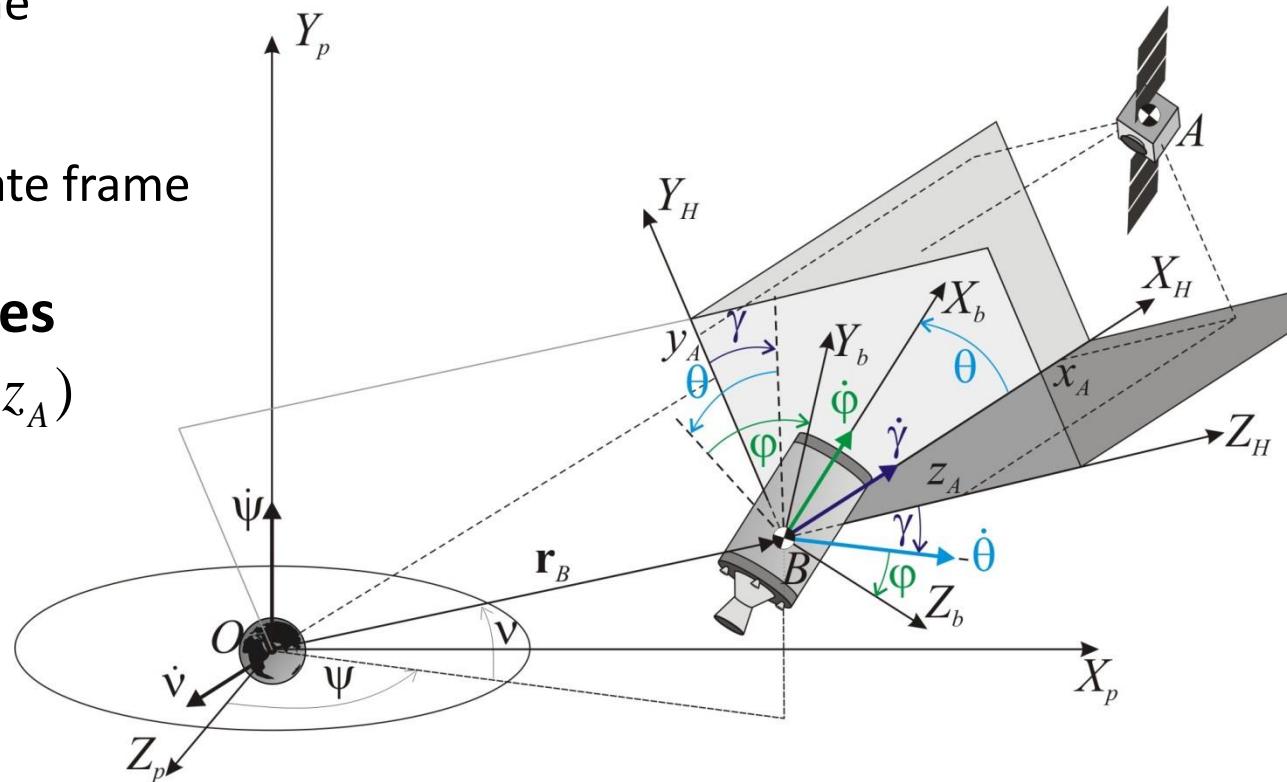
$OX_pY_pZ_p$ - inertial frame

$OX_bY_bZ_b$ - body frame

$OX_HY_HZ_H$ - Hill coordinate frame

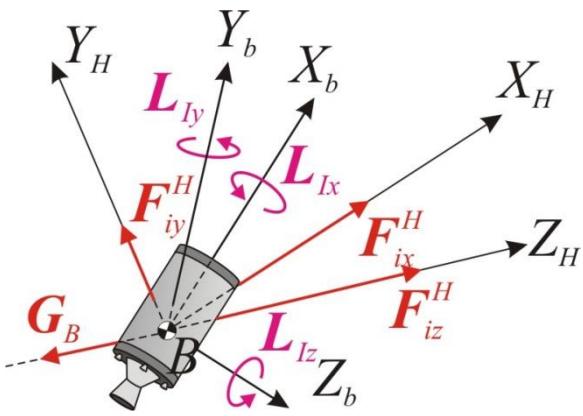
Generalized coordinates

$$\mathbf{q} = ((r, \nu, \psi, \dot{\psi}), (\theta, \phi, \dot{\theta}, \dot{\phi}), y_A, z_A)$$



$$x_A = d = \text{const}, \quad y_A = 0, \quad z_A = 0$$

Object's center of mass motion



$$m_B \ddot{\mathbf{r}}^p = \mathbf{G}_B^p + \mathbf{F}_I^p \quad (1)$$

$$\mathbf{G}_B^p = -\mu m_B \mathbf{r}^p r^{-3} \quad \text{Gravitational force}$$

$$\mathbf{F}_i^H = [F_{ix}^H, F_{iy}^H, F_{iz}^H]^T \quad \text{Ion beam force}$$

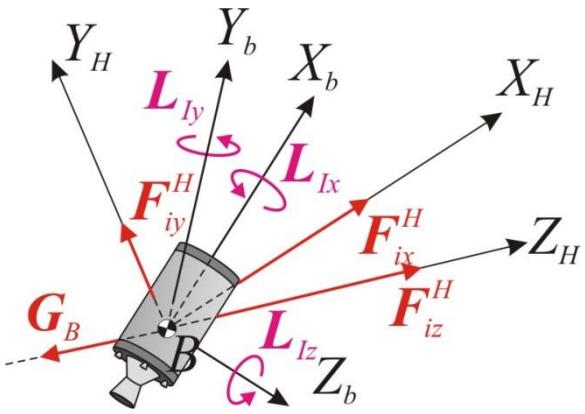
Equations of motion

$$\ddot{r} = r(\dot{\nu}^2 + \dot{\psi}^2 \cos \nu^2) - \frac{\mu}{r^2} + \frac{F_{iz}^H}{m_B}, \quad (2)$$

$$\ddot{\psi} = \frac{2\dot{\psi}\dot{\nu} \sin \nu}{c \cos \nu} - \frac{2\dot{\psi}\dot{r}}{r} + \frac{F_{ix}^H}{rm_B \cos \nu}, \quad (3)$$

$$\ddot{\nu} = -\dot{\psi}^2 \sin \nu \cos \nu - \frac{2\dot{\nu}\dot{r}}{r} + \frac{F_{iy}^H}{rm_B}. \quad (4)$$

Object's attitude motion



$$\frac{d\mathbf{H}_B^b}{dt} + \boldsymbol{\omega}^b \times \mathbf{H}_B^b = \mathbf{L}_G^b + \mathbf{L}_I^b \quad (5)$$

$\mathbf{H}_B^b = [\mathbf{I}] \boldsymbol{\omega}^b$ Angular momentum vector

$[\mathbf{I}]$ Object's inertia matrix

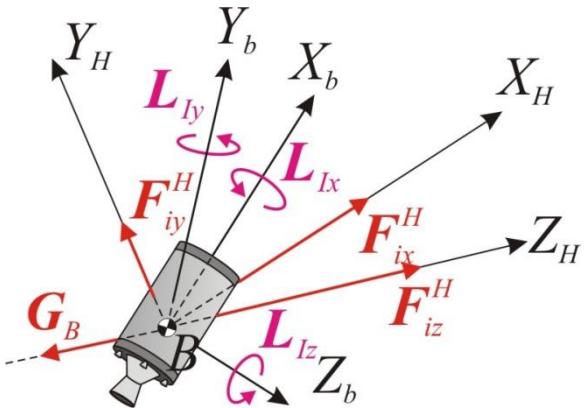
$\boldsymbol{\omega}^b = [\omega_x, \omega_y, \omega_z]^T$ Angular velocity

$\mathbf{L}_G^b = \frac{3\mu}{r^5} \mathbf{r}^b \times [\mathbf{I}] \mathbf{r}^b$ Gravity gradient torque

$\mathbf{L}_I^b = [L_{Ix}, L_{Iy}, L_{Iz}]^T$ Ion beam torque

$$\boldsymbol{\omega}^b = \dot{\mathbf{v}}^b + \dot{\boldsymbol{\psi}}^b + \dot{\boldsymbol{\gamma}}^b + \dot{\boldsymbol{\theta}}^b + \dot{\boldsymbol{\phi}}^b \quad (6)$$

Object's attitude motion in GEO



$$R = \bar{I}_x \omega_x, \quad G = R \cos \theta + (\omega_z \sin \varphi - \omega_y \cos \varphi) \sin \theta \quad (7)$$

$$\bar{I}_x = I_x / I, \quad I_y = I_z = I$$

$$\ddot{\theta} + \frac{(G - R \cos \theta)(R - G \cos \theta)}{\sin^3 \theta} = \frac{L_{Iz}^\varphi(\theta)}{I} \quad (8)$$

$$\dot{R} = L_{Ix}^\varphi(\theta) I^{-1} \quad (9)$$

$$\dot{G} = L_{Ix}^\varphi(\theta) I^{-1} \cos \theta - L_{Iy}^\varphi(\theta) I^{-1} \sin \theta \quad (10)$$

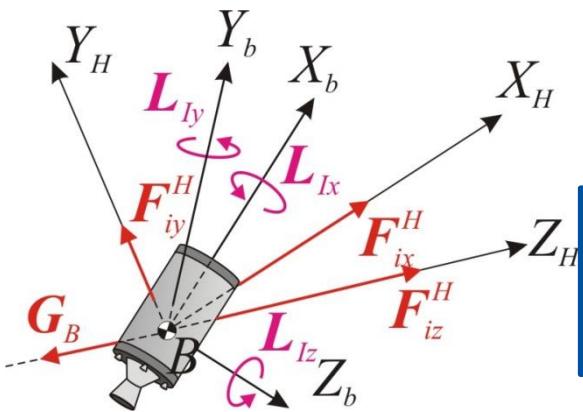
$$\dot{\gamma} = (G - R \cos \theta) \sin^{-2} \theta \quad (11)$$

$$\dot{\varphi} = R \bar{I}_x^{-1} - (G - R \cos \theta) \cos \theta \sin^{-2} \theta \quad (12)$$

$$L_{Ix}^\varphi = L_{Ix}, \quad L_{Iy}^\varphi = L_{Iy} \cos \varphi - L_{Iz} \sin \varphi,$$

$$L_{Iz}^\varphi = L_{Iy} \sin \varphi + L_{Iz} \cos \varphi$$

Object's attitude motion in GEO



$$L_{Ix}^\phi = L_{Iy}^\phi = 0, \quad L_{Iz}^\phi = uL_I^{\max} \sum_j^k b_j \sin j\theta \quad (13)$$

$u \in [0,1]$ Control parameter

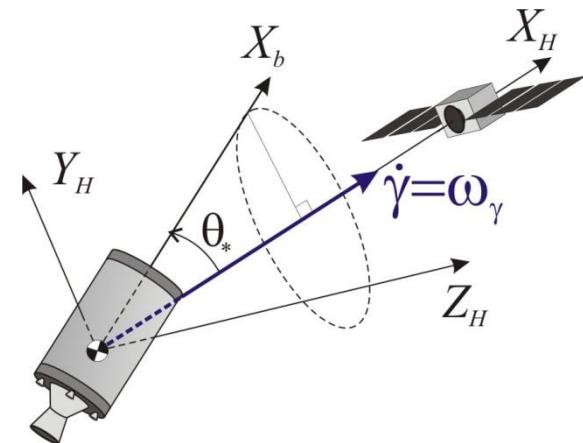
$$\ddot{\theta} + \frac{(G - R \cos \theta)(R - G \cos \theta)}{\sin^3 \theta} = \frac{uL_I^{\max}}{I} \sum_j^k b_j \sin j\theta \quad (14)$$

$$R = \text{const}, \quad G = \text{const}$$

$$\frac{\dot{\theta}^2}{2} + W(\theta) = E \quad (15)$$

$$W(\theta) = \frac{G^2 + R^2 - 2GR \cos \theta}{2 \sin^2 \theta} + \frac{uL_I^{\max}}{I} \sum_j^k \frac{b_j}{j} \cos j\theta \quad (16)$$

Object's equilibrium state



$$0 + \frac{(G_* - R_* \cos \theta_*)(R_* - G_* \cos \theta_*)}{\sin^3 \theta_*} = \frac{L_{I_z}^\varphi(\theta_*)}{I} \quad (8)$$

$$0 = \frac{G_* - R_* \cos \theta_*}{\sin^2 \theta_*} \quad (11)$$



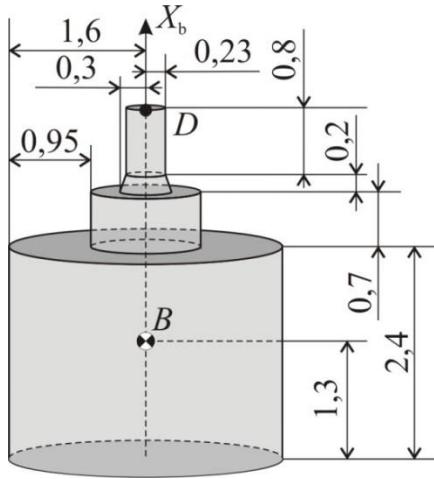
$$\theta_* = \arccos(G_* / R_*)$$

$$L_{I_z}^\varphi(\theta_*) = 0$$

(17)

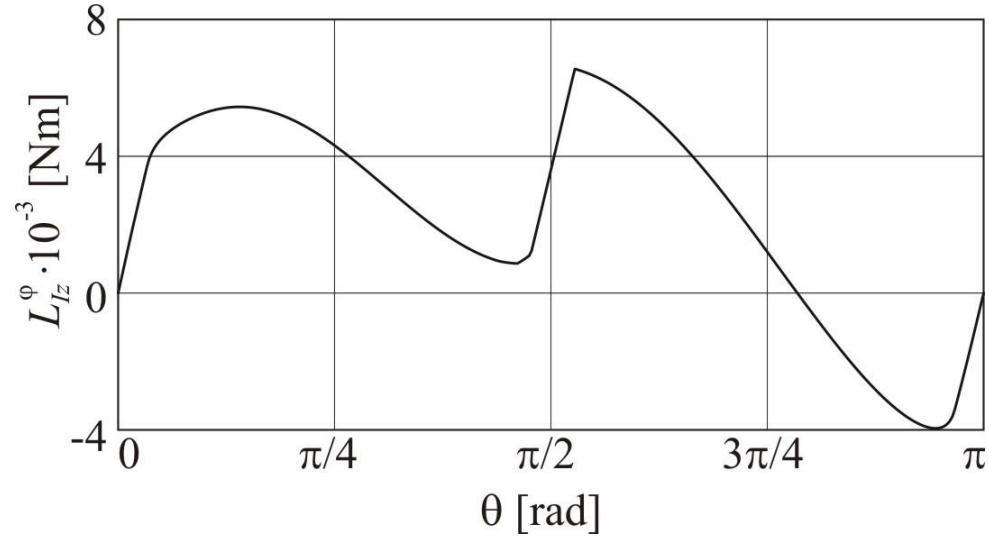
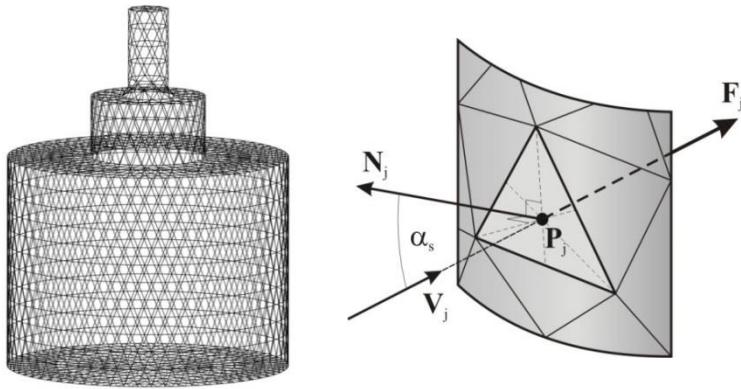
$$\theta_* \neq \arccos(G_* / R_*) \quad \dot{\gamma} = \frac{G_* - R_* \cos \theta_*}{\sin^2 \theta_*} = \omega_\gamma = \text{const}$$

System parameters



| Parameter | Value |
|-----------------------------------|------------------------------------|
| Mass m_B | 1100 kg |
| Moment of inertia I_x | 1400 kg m ² |
| Moments of inertia I_y, I_z | 2100 kg m ² |
| Plasma density n_0 | $2.6 \cdot 10^{16} \text{ m}^{-3}$ |
| Mass of the particle(xenon) m_0 | $2.18 \cdot 10^{-25} \text{ kg}$ |
| Ion velocity u_0 | 38000 m/s |
| Ion beam divergence angle | 15 deg |
| Distance d | 15 m |

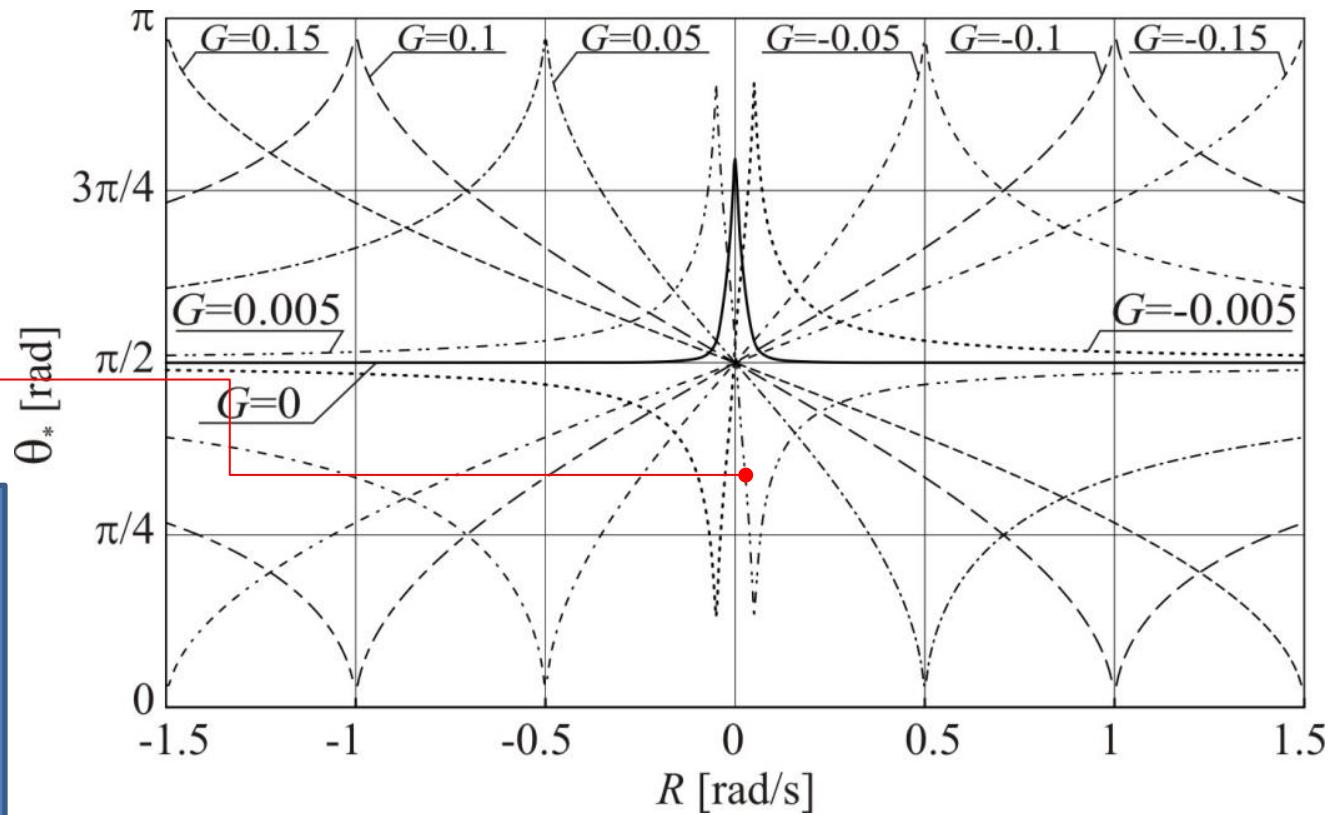
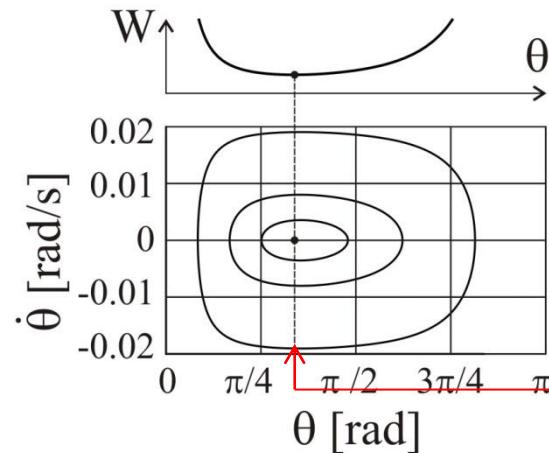
Ion beam torque



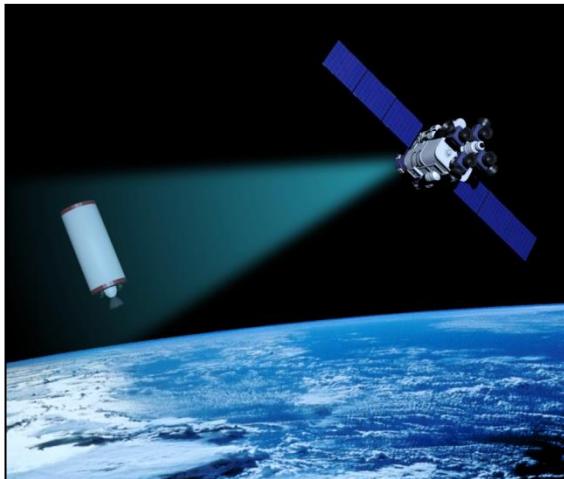
[1] A.P. Alpatov, S.V. Khoroshyllov, A.I. Maslova, Contactless de-orbiting of space debris by the ion beam. Dynamics and Control. — Kyiv: Akademperiodyka, 2019. — 170 p. DOI: [10.15407/akademperiodyka.383.170](https://doi.org/10.15407/akademperiodyka.383.170). (Chapter 3)

[2] V.S. Aslanov, A.S. Ledkov, Attitude motion of cylindrical space debris during its removal by ion beam, Mathematical Problems in Engineering. (2017) Article ID 1986374. DOI: [10.1155/2017/1986374](https://doi.org/10.1155/2017/1986374).

Uncontrolled attitude motion



Ion beam thrust control



$$L_{Iz}^\varphi = u L_I^{\max} \sum_j^k b_j \sin j\theta$$
$$u = \begin{cases} 1 + k(\theta - \theta_*) \dot{\theta} H[(\theta_* - \theta) \dot{\theta}], & \text{when } k(\theta - \theta_*) \dot{\theta} > -1; \\ 1, & \text{when } k(\theta - \theta_*) \dot{\theta} \leq -1; \end{cases}$$

$H[]$

Heaviside theta function

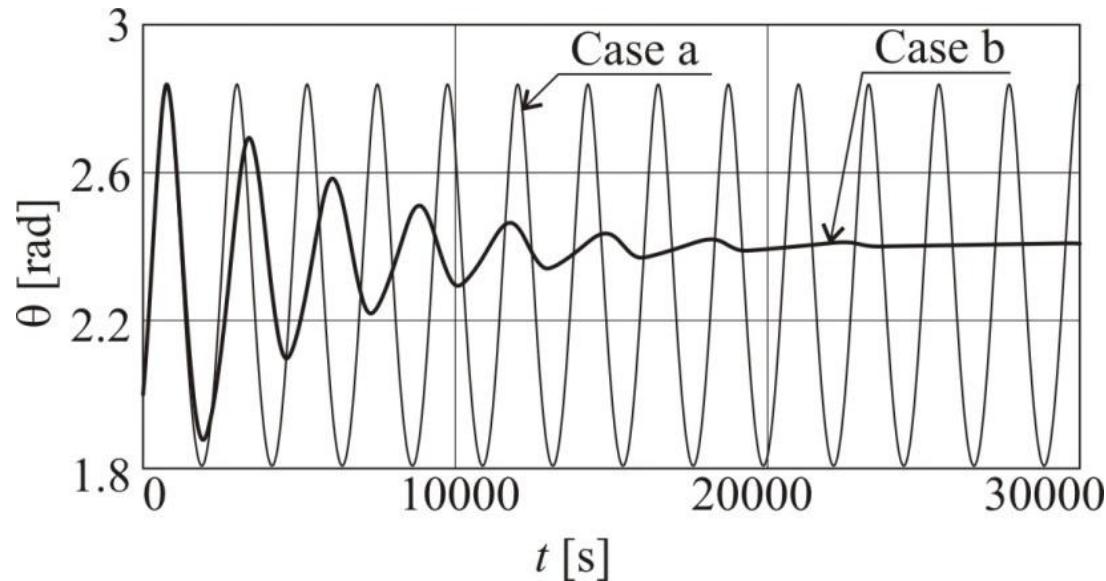
$$k = \frac{1}{\max_{[t-T,t]}(|(\theta - \theta_*) \dot{\theta}|)}$$

Control law parameter

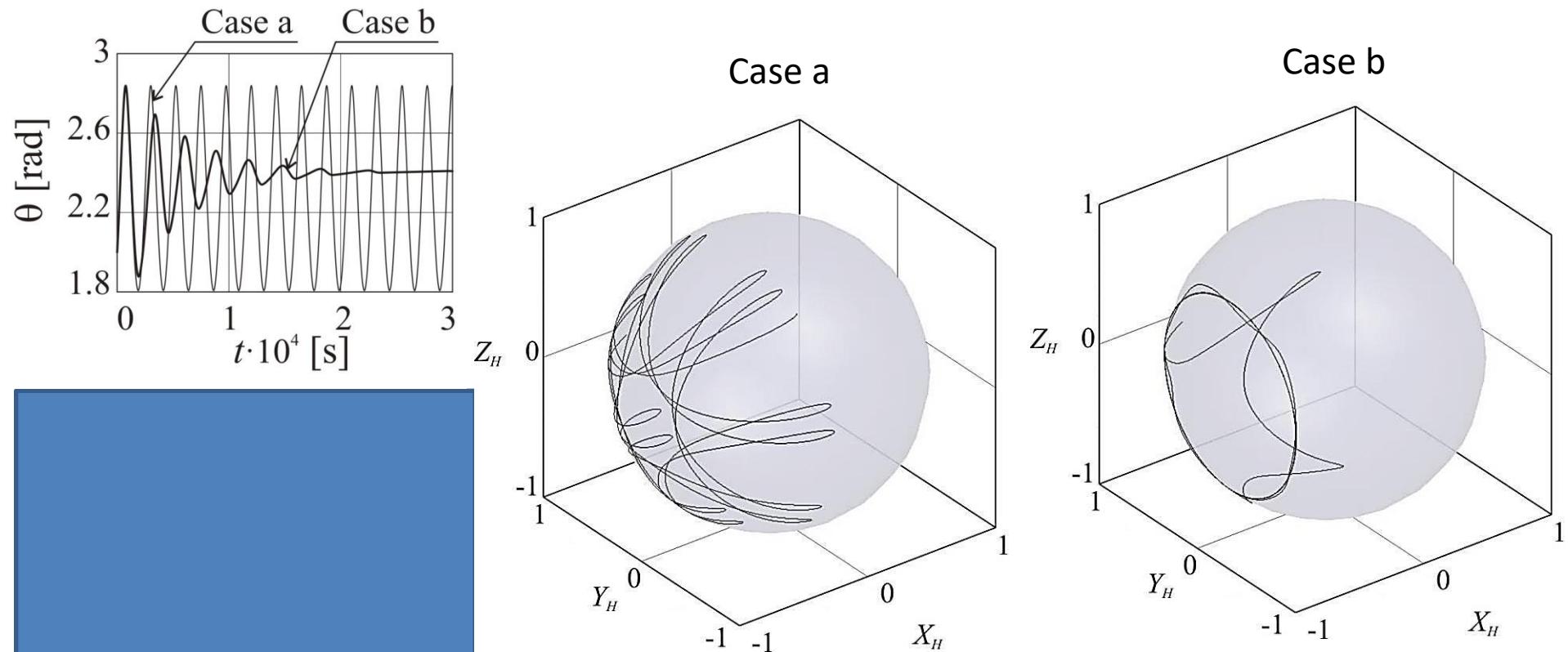
Numerical simulation result

Initial conditions

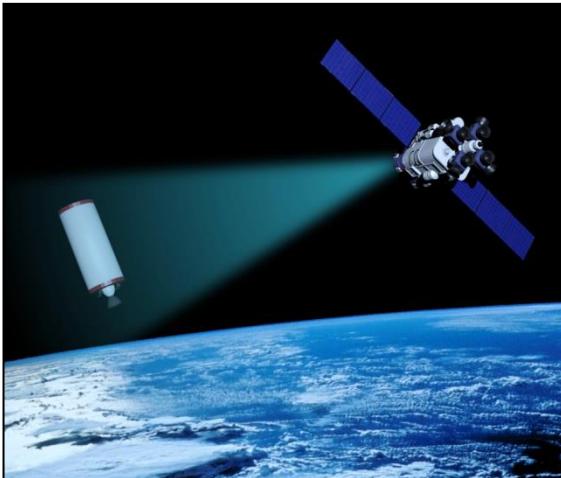
$$\omega_x = 0.001 \text{ rad/s}, \omega_y = \omega_z = 0, \theta_0 = 2 \text{ rad}, \gamma_0 = \varphi_0 = 0, \dot{\theta}_0 = 0.001 \text{ rad/s},$$
$$R = 6.6667 \cdot 10^{-4} \text{ rad/s}, G = -2.7743 \cdot 10^{-4} \text{ rad/s}, \theta_* = 2.4082 \text{ rad}$$



Numerical simulation result



Conclusions and results



- A mathematical model describing the spatial motion of a passive space object relative its center of mass was developed.
- Possible equilibrium positions was found.
- The ion beam thrust control law, which provides stabilization of the spatial oscillations of the object in the equilibrium position, was proposed.
- The effectiveness of the law was confirmed by the results of numerical simulations.



Thank you!

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